## Electronic Design

# Synchronous Boost Converter Powers High-Current LEDs Even at Low Input Voltages

To overcome the limitations of asynchronous dc-dc converters, designers can implement a synchronous boost LED controller to help deliver the required high output current for LEDs and LED strings thanks to its synchronous switching.

igh-power LEDs continue to proliferate in modern lighting systems, spanning automotive headlights, industrial/commercial signage, architectural lighting, and a variety of consumer electronics applications. The industry's transition toward LED technology is driven by the distinct advantages that solid-state lighting offers over conventional light sources—the high-efficiency conversion of electrical power to light output, as well as long operational life spans.

As LED lighting is incorporated into an expanding array of applications, the demand for higher LED currents for increased light output also grows. One of the biggest challenges for powering strings of high-current LEDs is maintaining high efficiency in the power-converter stage that's responsible for providing a well-regulated LED current. Inefficiency in the power converter presents itself in the form of unwanted heat, which originates from the switching elements of the current regulator circuitry.

A synchronous boost LED controller like the LT3762 developed by Analog Devices is designed to curtail the sources of efficiency loss common in high-power step-up LED driver systems (*Fig. 1*). Synchronous operation minimizes the losses normally incurred from the forward voltage drop of a catch diode in an asynchronous dc-dc converter, especially at low input voltages.

To improve low-input-voltage operation, an onboard dc-dc regulator provides 7.5 V to the gate-drive circuitry, even when the input drops below 7.5 V. The result of having a strong gate-drive voltage source at low input voltages is



1. The LT3762 demonstration circuit (DC2342A) powers up to 32 V of LEDs at 2 A over a wide input-voltage range. This demo circuit can easily be modified with additional MOSFETs and capacitors to increase the output power.

that the MOSFETs generate less heat as the input voltage decreases, which extends the low end of the operational input range to 3 V.

This step-up LED controller can be configured to operate between 100-kHz and 1-MHz fixed switching frequen-



2. Shown is a 32-V, 2-A LT3762 boost LED driver.

cy, with optional  $-30\% \times f_{SW}$  spread spectrum frequency modulation to reduce switching-related EMI energy peaks. The LED controller can be run in a step-up, step-down, or step-up/step-down topology for powering LEDs. A high-side PMOS disconnect switch facilitates pulse-width-modulation (PWM) dimming and protects the device from potential damage when the LEDs are placed in an open-/short-circuit condition.

A synchronous boost LED controller with an internal PWM generator needs only a single capacitor and a dc voltage to set the frequency and pulse width for up to a 250:1 PWM dimming ratio. It can alternatively use an external PWM signal to achieve ratios as high as 3000:1. The schematic in *Figure 2* shows a demonstration circuit application (DC2342A) configured to power up to 32 V of LEDs at 2 A from an input voltage range of 4 to 28 V.

#### Synchronous Switching

In asynchronous dc-dc converter topologies, Schottky catch diodes are used as passive switches to simplify the control scheme of the converter to pulse-width modulating a single MOSFET. While this does simplify things from a control perspective, it limits the amount of current that can be delivered to the output.

Schottky diodes, like PN junction devices, experience a forward voltage drop before any current can pass through the device. As the power dissipated in the Schottky diode is the product of its forward voltage drop and current, conduction-related power dissipation can result in several watts of loss at excessive output-current levels. This results in the Schottky diode heating up, which causes inefficiencies in the converter.

A synchronous switching converter doesn't encounter the same output-current limitations as those experienced with asynchronous converters. That's because synchronous converters replace the Schottky diode with a second MOS-FET. Unlike Schottky diodes, MOSFETs don't have a forward voltage drop. Instead, MOSFETs feature a small resistance that's formed from drain to source when the device is fully enhanced.

The conduction losses incurred from a MOSFET are much lower than with Schottky diodes at high current, as the power lost is proportional to the product of the square of the current through the device and drain-source resistance. Even at the lowest full power input voltage of 7 V, the MOSFETs only experience a temperature increase of roughly 30°C (*Fig. 3*).

#### Low-Input-Voltage Operation

Another challenging region for high-power boost LED controllers occurs during low-input-voltage operation. Most boost dc-dc regulator ICs use an internal LDO voltage



3. Under identical test conditions and using similar component selection, the synchronous LT3762 (left) powers a 32-V string of LEDs at 2 A with far less temperature rise than observed in an asynchronous LT3755-2 circuit (right). This increase in thermal performance is attributed to replacing the Schottky catch diode with a synchronous MOSFET, which eliminates the loss caused by the forward voltage drop of the diode.

regulator powered from the input of the device to provide lower-voltage power to the analog and digital control circuitry within the IC.

Of the circuitry that draws power from the internal LDO regulator, the gate driver consumes the most power, and its performance is affected by fluctuations in the output of the LDO regulator. As the input voltage drops below the LDO output voltage, the LDO output begins to collapse, which limits the gate driver's ability to properly enhance the MOS-FETs. When MOSFETs aren't fully enhanced, they operate in a higher resistance state, causing them to dissipate power

in the form of heat as current is passed through the device.

Low-input-voltage operation in stepup converter topologies results in higher input current, which, when having to pass through a more resistive MOSFET device, exacerbates conduction losses. Depending on the gate-drive voltage of the regulator IC, this can severely limit the low-input-voltage range that the device can successfully achieve without overheating.

When an integrated buck-boost dc-dc regulator is available instead of an LDO regulator, the LED controller can provide 7.5 V to power the internal circuitry even when the input voltage is low. This buck-boost regulator only consumes three pins of the IC and requires only two additional components.

Compared to internal LDO controller devices, which have minimum input voltages of 4.5 V and 6 V, the LT3762 is able to extend its input operating range down to 3 V (*Fig. 4*). The 7.5-V output of the buck-boost converter supplies power to the gate driver and allows for 6-V/7-V gate-drive MOSFETs to be used. Higher gate-drive voltage MOSFETs tend to have lower drain-source resistances and (barring switching losses) operate more efficiently than their lower gate-drive-voltage counterparts.

### **Flexible Topologies**

Many boost LED drivers can be reconfigured to power LEDs in a step-up configuration as well as a step-down



4. A 32-V, 2-A LT3762 LED driver maintains high efficiency over a wide input range. Low VIN foldback helps avoid excessive switch/inductor currents. Asynchronous switching starts at 24-V input.

(buck mode), and step-up/step-down (buck-boost mode and boost-buck mode). Of these boost-converter topology variants, the boost-buck mode configuration offers the ability to operate as a step-up/ step-down converter with the added benefit of low EMI operation. This topology utilizes two inductors, one input facing and the other output facing, to aid in filtering noise generated by switching. These inductors help suppress EMI from coupling to the input supply and other devices that may be connected, as well as the LED load.

Additional circuitry can be added on to the boost-buck mode topology to offer short-circuit protection of the LED<sup>-</sup> node to GND. The schematic in *Figure 5* shows a boost-buck mode configuration that adds this protection circuitry.

In the event that LED<sup>-</sup> is shorted to GND, M4 is forced to turn off, blocking the conduction path to the input through the inductors and preventing excessive current draw. When M4 is forced to turn off, D3 pulls the EN/UVLO pin low to stop the converter from switching until the short-circuit has been removed. Adding this protective circuitry used in conjunction with built-in open-/short-circuit detection results in a robust solution capable of surviving a variety of fault conditions in harsh environments.

Conclusion

Asynchronous boost converters often struggle to provide high output current without experiencing substantial power losses and heating of the catch diode under normal operation. In addition to loss generated by the Schottky diode, such converters struggle to maintain maximum power output capabilities as the input voltage decreases, which limits the power delivery across the input range.

Asynchronous dc-dc converters simply aren't suited for higher power levels, and a synchronous switching scheme must be implemented to meet application specifications. A synchronous boost LED controller addresses the issues of delivering high output current with its synchronous switching, is capable of operating at much lower input voltages thanks to its onboard dc-dc converter, and has the flexibility to be used in a variety of circuit topologies.

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#### 1 40 1 kΩ 5. This is a 25-V,sw 1.5-A boost-buck configuration of the LT3762 with D4 additional LED- to GND short-circuit protection. 1 ΜΩ **ξ**10 kΩ TT LED M4 D3 **D**2 L2 15 uH 4.7 μF ×3 RSNS1 EN/UVLO 7 L1 6 mΩ M3 LED<sup>4</sup> V<sub>IN</sub>\_ 4 V to 28 V 10 µH T T I 150 mΩ 4.7 µF ≺2 100 uE 10 uF 499 kO 1 µF MΩ 499 M2 D1 0.1 µF VIN SNSP SNSN SW BOOST Q1 LED 205 kΩ EN/UVLO 226 kQ M1 100 kΩ BG 36.5 kΩ CTRL1 TG FB CTRL2 Analog DIM ISF DIM 100 kΩ ₹ 100 kΩ ₹ 102 kΩ LT3762 ISN VREF PWMTG OPENI ED L3 **Open LED Fault** AUXSW2 SHORTLED Short LED Fault 47 µH 100 kΩ Ş 100 kΩ AUXSW1 INTVcc 0.1 µF 10 µF AUXBST SSFM D1-D3: Nexperia PMEG6010EJ SSFM On D4: Central CMDZ6L2 PWM SSEM Off L1: Coilcraft XAL1010-103ME On RT L2: Coilcraft XAL 5050-153ME External PWM DIM Ext 28.0 kΩ GND L2: Wurth 74408942470 SS Int M1, M2: Infineon BSC066N06NS 0.1 uE 3.3 kΩ M3, M4: Vishay Si7415DN 470 nF Q1: Zetex FMMT591A 4.7 nF Q2: Zetex FMMT491 RSNS1: Susumu KRL6432E-M-R006-F